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<sup>2</sup>Work supported by Department of Energy contract DE-AC03-76SF00515.

where  $\phi$  and  $\psi$  are horizontal and vertical opening angles, respectively. As is clear from eq.(1), the radiation is symmetric between  $\phi$  and  $\psi$  up to the second order. Usual equation, for example, that used in Refs. [5, 6] is not ready to calculate the horizontal opening angle, because the opening angle and the sweep angle are identified.

Here  $P$  is the power (energy/time),  $\omega_0 = c/p$  and the  $\theta$  is an angle

$$\theta^2 = \phi^2 + \psi^2,$$

$$(1) \quad \frac{dP}{d\omega d\phi d\psi} = \frac{4\pi^2 \omega^2}{h\alpha} \int_{-\infty}^{\infty} d\tau (\theta^2 - \frac{4}{\omega_0^2 \tau^2}) \cos \left[ \omega \tau \left\{ \frac{\gamma^{-2}}{\gamma^{-2} + \theta^2} + \frac{2}{24} \frac{\omega_0^2 \tau^2}{\omega^2} \right\} \right]$$

**Power Spectrum** Let us start with an equation in Ref.[4], which reads

## 2 Classical Formulae

Recently, a paper[3] was published on the general formalism for calculating the equilibrium envelope matrix based on the envelope formalism. This formalism is suited particularly for a numerical calculation. Also, an extension of the radiation integrals were made. The opening angle, however, were not included, because the effect is known tiny. In this paper, we apply the envelope formalism to this effect just for the sake of the completeness. Although the effect is tiny for realistic ring parameters, present and near future, it is still interesting to do so and may be important for future extreme machines.

taking into account the correlation between energy ( $\gamma$ ) and the opening angle ( $\psi$ ). The synchrotron radiation has an angle with respect to the velocity of the emitting particle. This angle is called the vertical opening angle. The effect of the vertical opening angle on the vertical emittance was roughly evaluated in Ref.[1]. In Ref.[2], it was done more carefully,

## 1 Introduction

The photons emitted by the synchrotron radiation are distributed transversely around the axis of the electron motion. This effect is treated in the envelope formalism. Radiation integrals are extended also. The effect is tiny for the damping rings of the future linear colliders.

## Effects of the Opening Angles to the Emittances<sup>2</sup>

In other words, the horizontal angle is usually integrated away. This is natural if we are concerned with the radiation power seen by an observer located at a position outside the beam. We are here, however, interested in the reaction of the photon emission to the emitting particle. In this case, the usual integrated formula is not useful.

From Eq.(1) and the definition of the Airy function, Eq.(40), we obtain

$$(2) \quad \frac{dP}{d\omega d\phi d\psi} = \frac{\pi}{h\alpha} \omega \left(\frac{\omega_0}{\omega}\right)^{2/3} (2\theta^2 + \gamma^{-2}) A_2 \left(\frac{\omega_0}{\omega}\right)^{2/3} (\theta^2 + \gamma^{-2}) \left(\frac{\omega_0}{\omega}\right)^{2/3},$$

where use is made of Eq.(41). Using Eq.(42), it can be cast in a form

$$(3) \quad \frac{dP}{d\omega d\phi d\psi} = \frac{h\alpha}{\pi^2 \sqrt{3} \omega_0} \omega^2 (2\theta^2 + \gamma^{-2}) \sqrt{\theta^2 + \gamma^{-2}} K_{1/3} \left( \frac{3\omega_0}{2\omega} [\theta^2 + \gamma^{-2}]^{3/2} \right)$$

**Energy Spectrum** Integrating Eq.(2) over  $d\phi d\psi = \pi d\theta^2$ , we get the well-known expression

$$(4) \quad \frac{dP}{d\omega} = \frac{2\pi}{\sqrt{3}} h\alpha \gamma \omega_0 \xi F(\xi), \quad F(\xi) = \int_{\xi}^{\infty} K_{5/3}(\xi') d\xi',$$

where

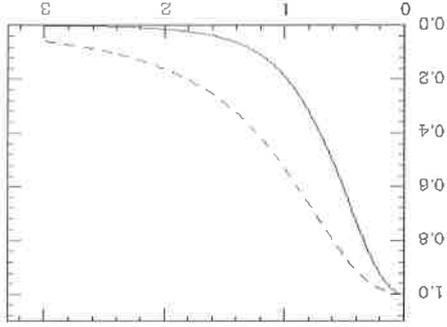
$$\xi = \frac{3\gamma^3 \omega_0}{2\omega}.$$

**Angular Spectrum** Integrating Eq.(3) over  $d\omega$ , and using Eq.(43), we get

$$(5) \quad \frac{dP}{d\phi d\psi} = \frac{\pi}{h\alpha} \omega_0^2 (2\theta^2 + \gamma^{-2}) \frac{d\phi d\psi}{2\theta^2 + \gamma^{-2}}$$

This is a monotonically decreasing function as shown in Fig.1. Note that this distribution has a non-Gaussian tail and decreases only slowly for large  $\theta$ .

Figure 1: Solid: Function  $(2X^2+1)/(X^2+1)^4$ , appearing in Eq.(5). Here  $X$  stands for  $\theta\gamma$ . Dashed: Function  $(2X^2+1)/(X^2+1)^{5/2}$ , appearing in Eq.(10).



**Total Power** Further integration of Eq.(4) over  $d\omega$  or Eq.(5) over  $d\phi d\psi$  lead to the total power (energy/time)

$$(6) \quad \int dP \equiv P_{tot} = \frac{2h\alpha c^2 \gamma^4}{3\rho^2}.$$

### 3 Quantum Formulae

**Photon Number** We are interested in the energy and angular distribution of each photon. The number of photons (or the number of photon emission) per unit time is given by [1]  $dN = dP/(h\omega)$ .

$$(7) \quad \frac{dN}{du d\phi d\psi} = \frac{\alpha}{n} \left(\frac{u_0}{n}\right)^{2/3} (2\theta^2 + \gamma^{-2}) A_1 \left(\frac{u_0}{n}\right)^{2/3} (\theta^2 + \gamma^{-2}),$$

$$(8) \quad = \frac{\alpha}{n} \frac{h\pi^2 \sqrt{3} u_0}{(2\theta^2 + \gamma^{-2}) \sqrt{\theta^2 + \gamma^{-2}}} K_{1/3} \left(\frac{3u_0}{2n} [\theta^2 + \gamma^{-2}]^{3/2}\right).$$

where  $u = h\omega$  and  $u_0 = h\omega_0$ .

From Eq.(4), just by dividing it by  $h\omega$ , we have

$$(9) \quad \frac{dN}{du} = \frac{\alpha}{n} \frac{\sqrt{3}\pi h\gamma^2}{u} F\left(\frac{n}{u}\right),$$

where

$$u_c = \frac{2\rho}{3hc\gamma^3}.$$

From Eq.(8), by completely parallel way to deriving Eq.(5), we get

$$(10) \quad \frac{dN}{du d\phi d\psi} = \frac{\alpha}{n} \frac{\sqrt{3} \pi d}{2\theta^2 + \gamma^{-2}} \frac{4}{\pi d} \frac{\pi d}{\theta^2 + \gamma^{-2}} \frac{5/2}{5/2}.$$

By integrating Eq.(9) over  $du$  or Eq.(10) over  $d\phi d\psi$ , we get the number of the photon emission (per second)

$$(11) \quad N_{tot} = \int dN = \frac{6}{5\sqrt{3} \alpha c \gamma} \rho.$$

**Energy and Angular Distribution of Photons** Once a photon is emitted, its energy and angular distribution is given by

$$(12) \quad \frac{dN}{du d\phi d\psi} f(u, \phi, \psi) du d\phi d\psi = \frac{N_{tot}}{4\pi} du d\phi d\psi.$$

We call the average over  $f$  the one-photon average and denote as

$$(13) \quad \langle A \rangle_1 \equiv \int A du d\phi d\psi.$$

The function  $n(u)$  used by Sands corresponds to  $N_{tot} f$ .

As easily seen, for any positive integer  $n$ ,

$$\langle u^n \phi \rangle_1 = \langle u^n \psi \rangle_1 = \langle u^n \phi \psi \rangle_1 = 0.$$

Interesting quantities are

$$(14) \quad \langle u^2 \rangle_1 = \frac{1}{55} \frac{N_{tot} 24\sqrt{3} \rho^3}{\alpha h^2 c^3 \gamma^7},$$

$$(15) \quad \langle u^2 \phi^2 \rangle_1 = \langle u^2 \psi^2 \rangle_1 = \frac{2}{13} \frac{N_{tot} 24\sqrt{3} \rho^3}{\alpha h^2 c^3 \gamma^5}.$$

$$I_n = \int \phi ds \left[ |V_{12}|^2 + |V_{14}|^2 B_{22} + |V_{16}|^2 B_{66} \right], \quad (22)$$

Here  $\alpha$ 's are the damping rates: these are unaffected by the opening angle and we can use the same expressions as in Ref.[3]. Now we have

$$(\varepsilon_n, \varepsilon_v, \varepsilon_w) = \frac{1}{2} \left( \frac{I_n}{I_n}, \frac{\alpha_n}{I_n}, \frac{\alpha_w}{I_n} \right). \quad (21)$$

Thus the perturbative "emittances" [3] become

$$B_{22} = B_{44} = \frac{N(\underline{\mathbf{x}}, s) \langle u^2 \phi^2 \rangle_1}{N(\underline{\mathbf{x}}, s) \langle u^2 \phi^2 \rangle_1}, \quad B_{66} = \frac{N(\underline{\mathbf{x}}, s) \langle u^2 \phi^2 \rangle_1}{N(\underline{\mathbf{x}}, s) \langle u^2 \phi^2 \rangle_1}. \quad (20)$$

$$B = \text{diag}(0, B_{22}, 0, B_{22}, 0, B_{66}), \quad (19)$$

vanishes so that we arrive at

**Radiation Integrals** If we employ the Frenet-Serret base, all of  $\underline{k}_x$ ,  $\underline{k}_y$  and  $\delta_k$  in Eq.(17)

$$B_0(s; \underline{\mathbf{x}}) = \frac{N(\underline{\mathbf{x}}, s) \langle u^2 \phi^2 \rangle_1}{N(\underline{\mathbf{x}}, s) \langle u^2 \phi^2 \rangle_1} \Delta_2 \text{diag}(0, \langle u^2 \phi^2 \rangle_1, 0, \langle u^2 \phi^2 \rangle_1, 0, 0, 0). \quad (18)$$

where  $\Delta = 1/(1 + \delta_k)$  and  $N = c^{-1} N_{tot} dl/ds$ . Here the first term is identical with the  $B$  matrix in Ref.[3], while  $B_0$  is the contribution from the opening angle

$$B(s; \underline{\mathbf{x}}) = \frac{N(\underline{\mathbf{x}}, s) \langle u^2 \phi^2 \rangle_1}{N(\underline{\mathbf{x}}, s) \langle u^2 \phi^2 \rangle_1} \begin{pmatrix} 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & \Delta_2 \underline{k}_x \underline{k}_y & 0 & 0 & 0 & 0 \\ 0 & 0 & \Delta_2 \underline{k}_x \underline{k}_y & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & \Delta_2 \underline{k}_x \underline{k}_y & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \end{pmatrix} + B_0(s; \underline{\mathbf{x}}). \quad (17)$$

Since  $\langle u \phi \rangle_1 = \langle u \psi \rangle_1 = 0$ , the damping matrix [3] is not affected at all by the opening angle. The diffusion matrix has a contribution

$$\xi(\underline{\mathbf{x}}) = -\frac{E_0}{n} \left( 0, \frac{k_x + \phi}{1 + \delta_k}, 0, \frac{k_y + \psi}{1 + \delta_k}, 0, 1 \right) \quad (16)$$

The diffusion Matrix We use the rectangular coordinate system. The stochastic variable  $\xi$  expressing the reaction of a photon emission to the canonical variables is

## 4 Emittances

As clear from Eq.(14) and Eq.(15),  $\langle u^2 \phi^2 \rangle_1$  is roughly  $\gamma^2$  times as large as  $\langle u^2 \phi^2 \rangle_1 = \langle u^2 \psi^2 \rangle_1$ . Thus the effect of the opening angle becomes smaller for rings with higher energy.

The Eq.(14) is well-known. The Eq.(15) was calculated in Ref.[2] for the vertical angle ( $\psi$ ) in different way. The calculation is easy if we start from Eq.(8) and integrate over  $n$  first.

$$\frac{\langle \delta z^2 \rangle_c}{\langle \delta z^2 \rangle_o} = \frac{\oint ds \gamma_z \eta_z^2 B_{66}^2}{\oint ds \gamma_z \eta_z^2 B_{66}^2} \approx \frac{\gamma_z^2 R^2}{\gamma_z^2 R^2} \quad (37)$$

Let us evaluate the effects of the opening angle to the emittances by using the smooth approximation. In the smooth approximation, we have  $\beta_z = \alpha_m R / v_s$ , where  $R$  is the mean radius,  $\alpha_m$  the momentum compaction factor and  $v_s$  the synchrotron tune. For the energy spread  $\langle \delta z^2 \rangle$ , we get

$$I_w = \oint ds \left[ \gamma_z^2 \eta_z^2 B_{22} + \frac{\gamma_z}{\beta_z} B_{66} \right], \quad (36)$$

$$I_v = \oint ds \left[ \frac{\beta_y}{\beta_z} B_{22} \right], \quad (35)$$

$$I_u = \oint ds \left[ \frac{\beta_x}{\beta_z} B_{22} + \frac{\gamma}{\mathcal{H}} B_{66} \right], \quad (34)$$

where  $\gamma_z = (1 + \alpha_z^2)^{1/2} / \beta_z$  and  $\mathcal{H} = \mathcal{H}_x$  and  $b$  is unity. In this case, Eqs.(22)-(24) are much simplified:  $(u, v, w)$  is identical with  $(x, y, z)$  and  $b$  is unity.

**Perfect Machines** Let us assume that the ring is perfect and the dispersions are zero in

Here  $|V_{16}|^2$  and  $|V_{36}|^2$  correspond to well-known terms and  $|V_{56}|^2$  is shown in Ref.[3].

$$|V_{56}|^2 = \frac{\beta_w}{2}. \quad (33)$$

$$|V_{54}|^2 = \frac{2\beta_w}{(1 + \alpha_w^2)\eta_w^2}, \quad (32)$$

$$|V_{52}|^2 = \frac{2\beta_w}{(1 + \alpha_w^2)\eta_w^2}, \quad (31)$$

$$|V_{36}|^2 = \frac{2\beta_u}{\eta_u^2 + (\alpha_u \eta_u - \beta_u \eta_u')^2} \equiv \frac{1}{2} \mathcal{H}_u, \quad (30)$$

$$|V_{34}|^2 = \frac{b^2 \beta_u}{2}, \quad (29)$$

$$|V_{32}|^2 = \frac{2\beta_u}{r_u^2 + (\alpha_u r_u + \beta_u r_u')^2} \equiv \frac{1}{2} \mathcal{G}_u, \quad (28)$$

$$|V_{16}|^2 = \frac{2\beta_u}{\eta_u^2 + (\alpha_u \eta_u - \beta_u \eta_u')^2} \equiv \frac{1}{2} \mathcal{H}_u, \quad (27)$$

$$|V_{14}|^2 = \frac{2\beta_u}{r_u^2 + (\alpha_u r_u - \beta_u r_u')^2} \equiv \frac{1}{2} \mathcal{G}_u, \quad (26)$$

$$|V_{12}|^2 = \frac{b^2 \beta_u}{2}, \quad (25)$$

integrals have simpler forms: Let us assume that the dispersions are zero in cavities. In this case, the radiation Here  $V$  is the diagonalizing matrix. (See Eqs.(96) - (102) in Ref.[3].)

$$I_w = \oint ds \left[ (|V_{52}|^2 + |V_{54}|^2) B_{22} + |V_{56}|^2 B_{66} \right]. \quad (24)$$

$$I_v = \oint ds \left[ (|V_{32}|^2 + |V_{34}|^2) B_{22} + |V_{36}|^2 B_{66} \right], \quad (23)$$

him.

P. Chen and T. Raubenheimer are acknowledged for useful discussions. He also thanks the members of the Accelerator Theory group of SLAC for their hospitality extended to

### Acknowledgements

We have extended the diffusion matrix  $B$  in the envelope formalism and the radiation integrals by including the opening angle effects. For usual parameters of the storage and damping rings, its effects are tiny. For more future machines with smaller emittances, linear or circular, the envelope formalism including the opening angle effects should play an important role. The same formalism can also be applied to evaluate the emittance growth effects due to other incoherent processes: the scattering by the residual gas, for example.

## 5 Discussions

The vertical emittances due to the opening angle is less than 2% of the specified values.

	$L_b$ (m)	$L_w$ (m)	$\beta_b^y$ (m)	$\beta_w^y$ (m)	$\rho_b$ (m)	$\rho_w$ (m)	$\epsilon_y \times 10^{-13}$ (m)
JLC	29	9.6	3	2.6	4.6	2.5	1.5
ATF	35.8	12	6	5.3	5.7	2.6	1.2
NLC	29	9.6	3	2.6	4.6	2.5	1.5
JLC	35.8	12	6	5.3	5.7	2.6	1.2
ATF	29	9.6	3	2.6	4.6	2.5	1.5
NLC	35.8	12	6	5.3	5.7	2.6	1.2

$f_w = \frac{B_r}{R_s}$   
 $\beta_b^y$  1.7 nm 2.0 nm 6.8 nm  
 $\beta_w^y$  30 30 30  
 $\beta_b^x$  13.4 15.5 9.2  
 $\beta_w^x$  30 30 30

The last approximation applies when the damping time is dominated by the wigglers. The vertical emittances of some damping rings are evaluated as follows:

$$\epsilon_y = \frac{13}{55} C_q \frac{\int ds \frac{\rho^2}{\beta_y^3}}{\int ds \frac{\rho^2}{\beta_y}} \approx 0.9 \times 10^{-13} \times \frac{\rho_w}{\beta_w^y} \quad (\text{m} \cdot \text{rad}) \quad (39)$$

$\epsilon_y \approx 2$

Lastly the vertical emittance  $\epsilon_y$  is [2]

$$\frac{\epsilon_C^x}{\epsilon_C^y} \approx \frac{\beta_x B_{22}}{\beta_y B_{11}} = \frac{H B_{66}}{26 \beta_x} = \frac{55 H \gamma^2}{1} \quad (38)$$

Similarly, the contribution to the horizontal emittance is angle contribution is extremely small. Here the suffix O and C mean "opening angle contribution" and "conventional scheme", respectively and a use is made of  $\alpha_m \approx n_x/p$  in the last approximate equality. The opening

## A Airy and related functions

$$Ai(x) = \frac{1}{\sqrt{3}} \int_{-\infty}^{\infty} du \cos[ux + \frac{u^3}{3}] \quad (40)$$

$$Ai''(x) - xAi(x) = 0 \quad (41)$$

$$Ai(x) = \frac{1}{\sqrt{3}} \sqrt{\frac{x}{3}} K_{1/3}(\frac{2}{3}x^{3/2}), \quad Ai'(x) = -\frac{1}{\sqrt{3}} \frac{\sqrt{x}}{x} K_{2/3}(\frac{2}{3}x^{3/2}) \quad (42)$$

$$\int_0^{\infty} t^{\mu-1} K_{\nu}(at) dt = 2^{\mu-2} a^{-\mu} \Gamma\left(\frac{\mu+\nu}{2}\right) \Gamma\left(\frac{\mu-\nu}{2}\right) \quad (43)$$

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